

In the Specification:

Please replace the paragraph beginning at page 2, line 13, with the following amended paragraph:

-- ~~European patent publication 0,728,803~~ United States Patent 5,804,636 discloses a method for making a silicic-acid containing rubber base composition of the kind mentioned initially herein. In a first stage of the method, the composition ingredients of rubber, silicic acid and additional additives except the vulcanization ingredients are mixed with each other at a temperature in the range of 165°C to 170°C in a first mixer. After mixing the composition ingredients, the composition is removed from the first mixer, cooled and transferred to a second mixer. In the second mixer, silane is added to the composition and the composition is mixed to completion at a temperature of 135°C and the silane reacts with the silicic acid. Because of the high temperature of the composition in the first mixer, it is ensured that the composition ingredients disperse rapidly and well; whereas, a thermal decomposition of the silane is avoided by maintaining the temperature of 135°C in the second mixer. Furthermore, by using two mixers, the advantage is provided that, at the same time, a rubber base composition without silane is mixed in the first mixer and, in the second mixer, a rubber base composition with silane can be mixed to the end. In this way, the expenditure of time for producing a rubber base composition containing silicic acid is shortened. --

Please replace the paragraph beginning at page 3, line 5, with the following amended paragraph:

-- It is, however, noted that in the method set forth in ~~European patent publication 0,728,803~~, United States Patent 5,804,636, the silicic-acid containing rubber base

composition must be cooled down in an intermediate step which leads to an additional expenditure of time and storage. --

Please replace the paragraph beginning at page 4, line 27, with the following amended paragraph:

-- An advantage of the invention is especially that the method can be executed with a reduced expenditure as to both time and space because an intermediate storage and cooling of the rubber base composition after separating the same from the first mixer is unnecessary. A further advantage of the invention is that all composition ingredients of the rubber base composition are introduced into the first mixer and therefore also only stationary metering devices are needed in the region of the first mixer. Furthermore, it is ensured that the individual composition ingredients in the rubber base composition are present in the correct amounts. (At this point, it is noted that in the method known from ~~European patent publication 0,728,803~~, United States Patent 5,804,636, the above is not ensured. Accordingly, it can happen that, when separating the rubber base composition from the first mixer, composition ingredients remain in the first mixer so that the rubber base mixture in the second mixer is supplied with too much silane; on the other hand, it can be that residual amounts from previous mixture operations are separated from the first mixer with the rubber base composition so that the rubber base composition is supplied with too little silane in the second mixer.) --

Please replace the paragraph beginning at page 8, line 21, with the following amended paragraph:

-- According to another embodiment of the invention, the second mixer has a greater fill volume than the first mixer. Preferably, the fill volume of the second mixer is greater than the fill volume of the first mixer by 20 to 60%. Use is made of this embodiment when the first mixer is a ram mixer and the

second mixer is a ramless mixer. The advantage of this embodiment becomes understandable when the following is considered. In a ram mixer, the composition is pressed continuously by the ram between the rotors of the mixer so that an excellent through mixing of the composition is ensured. In contrast, in a ramless mixer, the problem is present that the composition leaves the region between the rotors because of the rotation thereof and, because of the non-present ram, cannot again come into this region. A thorough mixing of the composition ~~in~~ is then no longer ensured. This problem is that much greater the smaller the fill volume is of the mixer. The advantage of the embodiment is therefore that, because of the greater fill volume of the second mixer, virtually the entire composition can be accommodated in the region between the rotors and is almost always disposed in this region so that an excellent through mixing of the rubber base composition in the second mixer is ensured even without the ram. --

Please replace the paragraph beginning at page 10, line 27, with the following amended paragraph:

-- A ramless second mixer 18 is mounted below the first mixer 2. The second mixer 18 has a mixing chamber 24 having a fill volume greater than preferably 20 to 60% than the mixing chamber 4 of the first mixer 2. The second mixer 18 includes an inlet opening 20 and rotors 22 which are preferably interengaging rotors and are disposed in the mixing chamber 24. The outlet opening 26 of the second mixer 18 is closed by a movable saddle 28 which, in a manner known per se, can be flipped into an ~~open position~~ about a horizontal axis from the closed position shown in FIG. 1 into an open position. In the open position, the saddle clears the outlet opening 26 of the mixture chamber 24. --

Please replace the paragraph beginning at page 14, line 20, with the following amended paragraph:

-- FIG. 3 shows a diagram wherein the temperature  $T$  in the mixers (2, 18) is plotted as a function of time  $t$ . Here, a composition forms the basis wherein the uniform distribution of the composition ingredients takes a first time span  $t_1$  and the almost complete reaction of the silicic acid with the silane takes a second time span  $t_2$ , which is longer than the first time span  $t_1$ . In this case too, it is possible to match the dwell times of the composition in the mixers (2, 18) in such a manner with respect to each other that they are identical as is explained hereinafter (here, the left part of the diagram shows the time-dependent temperature trace for the composition in the first mixer 2 and the right part of the diagram shows the time-dependent temperature trace for the composition in the second mixer 18). In the first mixer 2, the composition ingredients are introduced at the same time or at time intervals and dispersed over the time span  $t_1$ . Here, the temperature of the composition ingredients is increased starting from room temperature to a temperature of approximately 130°C. At this temperature, the silicic acid starts to react intensively with the silane. After the first time span  $t_1$  has elapsed, the temperature of the composition is increased to a desired temperature in the temperature range of 130°C to 180°C. In total, the temperature of the composition is held in the first mixer 2 over a time span  $t_3 = (t_2 - t_1)/2$  in the temperature range of 130°C to 180°C. The dwell duration of the composition in the first mixer 2 amounts to a total  $(t_1 + t_2)/2$ . --

Please replace the paragraph beginning at page 15, line 16, with the following amended paragraph:

-- After the elapse of time span  $t_3$ , the composition is transferred directly from the first mixer 2 into the second mixer 18 without intermediate storage. In the second mixer 18, the temperature of the composition lies in the temperature range of 130°C to 180°C over the entire dwell duration  $(t_1 + t_2)/2$  of

the composition in the second mixer; that is, the dwell duration of the composition in the second mixer 18 corresponds to the dwell duration of the composition in the first mixer 2. Preferably, the temperature of the composition in the second mixer is held constant at the value which the composition had assumed in the transfer from the first mixer into the second ~~mixer 18~~ mixer 18. --